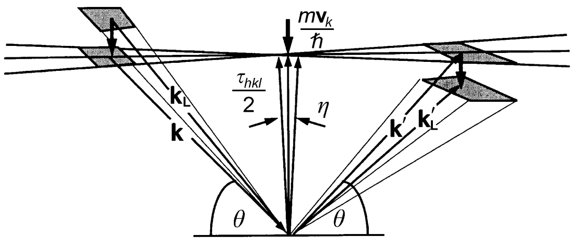
International Tables for Crystallography (2006). Vol. C, Table 4.4.2.2, p. 435.

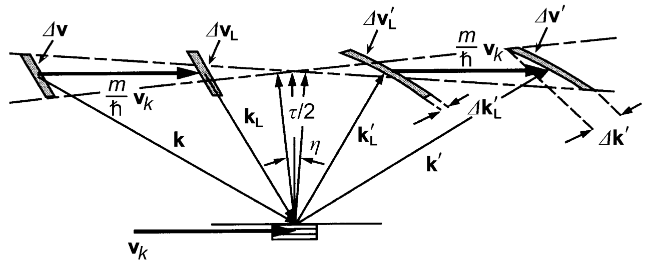
eter, first conceived by Brockhouse (1958). A pulse of monochromatic neutrons is obtained when the reciprocal-lattice vector of a rotating crystal bisects the angle between two collimators. Effectively, the neutron **k** vector is changed in both direction and magnitude, depending on whether the crystal is moving towards or away from the neutron. For the rotating crystal, both of these situations occur simultaneously for different halves of the crystal, so that the net effect over the beam cross section is that a wider energy band is reflected than from the crystal at rest, and that, depending on the sense of rotation, the beam is either focused or defocused in time (Meister & Weckerman, 1972).

The Bragg reflection of neutrons from a crystal moving parallel to its lattice planes is illustrated in Fig. 4.4.2.3(*b*). It can be seen that the moving crystal selects a larger Δk than the crystal at rest, so that the reflected intensity is higher. Furthermore, it is possible under certain conditions to orientate the diffracted phase-space volume orthogonal to the diffraction vector. In this way, a monochromatic divergent beam can be obtained from a collimated beam with a larger energy spread. This provides an elegant means of producing a divergent beam with a sufficiently wide momentum spread to be scanned by the Doppler crystal of a backscattering instrument (Schelten & Alefeld, 1984).

Finally, an alternative method of scanning the energy of a monochromator in backscattering is to apply a steady but uniform temperature variation. The monochromator crystal must have a reasonable thermal expansion coefficient, and care has to be taken to ensure a uniform temperature across the crystal.



(*a*)



(*b*)

Fig. 4.4.2.3. Momentum-space representation of Bragg scattering from a crystal moving (*a*) perpendicular and (*b*) parallel to the diffracting planes with a velocity $\mathbf{v}_k$. The vectors $\mathbf{k}_L$ and $\mathbf{k}_L'$ refer to the incident and reflected wavevectors in the laboratory frame of reference. In (*a*), depending on the direction of $\mathbf{v}_k$, the reflected wavevector is larger or smaller than the incident wavevector, $\mathbf{k}_L$. In (*b*), a larger incident reciprocal-space volume, $\Delta\mathbf{v}_L$, is selected by the moving crystal than would have been selected by the crystal at rest. The reflected reciprocal-space element, $\Delta\mathbf{v}_L'$, has a large divergence, but can be arranged to be normal to $\mathbf{k}_L'$, hence improving the resolution $\Delta\mathbf{k}_L'$.

Table 4.4.2.2. *Neutron scattering-length densities, Nb_{coh}, for some commonly used materials*

Material	Nb (10^{-6} Å^{-2})
^{58}Ni	13.31
Diamond	11.71
Nickel	9.40
Quartz	3.64
Germanium	3.62
Silver	3.50
Aluminium	2.08
Silicon	2.08
Vanadium	−0.27
Titanium	−1.95
Manganese	−2.95

4.4.2.4. *Mirror reflection devices*

The refractive index, n, for neutrons of wavelength λ propagating in a nonmagnetic material of atomic density N is given by the expression

$$n^2 = 1 - \frac{\lambda^2 Nb_{\rm coh}}{\pi,} \qquad (4.4.2.4)$$

where $b_{\rm coh}$ is the mean coherent scattering length. Values of the scattering-length density $Nb_{\rm coh}$ for some common materials are listed in Table 4.4.2.2, from which it can be seen that the refractive index for most materials is slightly less than unity, so that total external reflection can take place. Thus, neutrons can be reflected from a smooth surface, but the critical angle of reflection, γ_c, given by

$$\gamma_c = \lambda\left(\frac{Nb_{\rm coh}}{\pi}\right)^{1/2}, \qquad (4.4.2.5)$$

is small, so that reflection can only take place at grazing incidence. The critical angle for nickel, for example, is 0.1°Å^{-1}.

Because of the shallowness of the critical angle, reflective optics are traditionally bulky, and focusing devices tend to have long focal lengths. In some cases, however, depending on the beam divergence, a long mirror can be replaced by an equivalent stack of shorter mirrors.

4.4.2.4.1. *Neutron guides*

The principle of mirror reflection is the basis of neutron guides, which are used to transmit neutron beams to instruments that may be situated up to 100 m away from the source (Christ & Springer, 1962; Maier-Leibnitz & Springer, 1963). A standard neutron guide is constructed from boron glass plates assembled to form a rectangular tube, the dimensions of which may be up to 200 mm high by 50 mm wide. The inner surface of the guide is coated with approximately 1200 Å of either nickel, ^{58}Ni ($\gamma_c = 0.12°$Å^{-1}), or a 'supermirror' (described below). The guide is usually evacuated to reduce losses due to absorption and scattering of neutrons in air.

Theoretically, a neutron guide that is fully illuminated by the source will transmit a beam with a square divergence of full width $2\gamma_c$ in both the horizontal and vertical directions, so that the transmitted solid angle is proportional to λ^2. In practice, owing to imperfections in the assembly of the guide system, the divergence profile is closer to Gaussian than square at the end of a long guide. Since the neutrons may undergo a large number of reflections in the guide, it is important to achieve a high reflectivity. The specular reflectivity is determined by the surface roughness, and typically values in the range 98.5 to 99% are