8.3. Constraints and restraints in refinement

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In Chapter 8.1, the method of least squares is discussed as a technique for fitting a theoretical model that contains adjustable parameters to a set of observations. The discussion is very general and contains very little mention of what sorts of quantities the observations are or what the model represents. In crystallography, the model is a crystal, which is constructed from identical unit cells that contain atoms, and which diffracts X-rays, neutrons or electrons in a manner that is characteristic of the arrangement of those atoms. The sample may be either a single crystal or a polycrystalline powder, and the observations are diffracted intensities, which may be fitted directly, as in the Rietveld method for powders (see Chapter 8.6; also Rietveld, 1969), or converted to derived quantities such as integrated intensities, squared moduli of structure amplitudes, or the structure amplitudes themselves. The model generally contains a scale factor and may contain parameters describing other experimental effects, such as extinction. Each atom in the unit cell requires three parameters to describe its mean position and various parameters to describe random deviations from that position owing to thermal motion or disorder. Models that treat each atom independently, however, do not allow for the fact that a great deal more is known about a crystal initially than simply its chemical composition. Atoms have fairly definite sizes and tend to occupy sites whose surroundings conform to a rather limited set of common configurations. In this chapter, we discuss ways of using this additional information. First, we shall discuss the use of constraints to reduce the number of parameters that must be varied and account for relationships among parameters that are dictated by the laws of chemistry and physics. Then we shall discuss the use of restraints, which effectively add to the number of observations that must be fitted by the model.

8.3.1. Constrained models

The techniques of least squares are applicable for refining almost any model, but the question of the suitability of the model remains. The addition of parameters may reduce the residual disagreement, but lead to solutions that have no physical or chemical validity. Addition of constraints is one method of constricting the solutions.

8.3.1.1. Lagrange undetermined multipliers

The classical technique for application of constraints is the use of Lagrange undetermined multipliers, in which the set of p parameters, x_j , is augmented by p-q (q < p) additional unknowns, λ_k , one for each constraint relationship desired. The problem may be stated in the form: find the minimum of

$$S = \sum_{i=1}^{n} w_i [y_i - M_i(\mathbf{x})]^2, \qquad (8.3.1.1a)$$

subject to the condition

$$f_k(\mathbf{x}) = 0 \quad (k = 1, 2, \dots, p - q).$$
 (8.3.1.1b)

This may be shown (Gill, Murray & Wright, 1981) to be equivalent to the problem: find a point at which the gradient of

$$S' = \sum_{i=1}^{n} w_i [y_i - M_i(\mathbf{x})]^2 + \sum_{k=1}^{p-q} \lambda_k f_k(\mathbf{x})$$
 (8.3.1.2)

vanishes. Solving for the stationary point leads to a set of simultaneous equations of the form

$$\partial S'/\partial x_j = \partial S/\partial x_j + \sum_{k=1}^{p-q} \lambda_k \partial f_k(\mathbf{x})/\partial x_j = 0$$
 (8.3.1.3*a*)

and

$$\partial S'/\partial \lambda_k = f_k(\mathbf{x}) = 0.$$
 (8.3.1.3b)

Thus, the number of equations, and the number of unknowns, is increased from p to 2p-q. In cases where the number of constraint relations is small, and where it may be difficult to solve the relations for some of the parameters in terms of the rest, this method yields the desired results without too much additional computation (Ralph & Finger, 1982). With the large numbers of parameters, and large numbers of constraints, that arise in many crystallographic problems, however, the use of Lagrange multipliers is computationally inefficient and cumbersome.

8.3.1.2. Direct application of constraints

In most cases encountered in crystallography, constraints may be applied directly, thus reducing rather than increasing the size of the normal-equations matrix. For each constraint introduced, one of the parameters becomes dependent on the remaining set, and the rank of the remaining system is reduced by one. For p parameters and p-q constraints, the problem reduces to q parameters. If the Gauss–Newton algorithm is used (Section 8.1.4), the normal-equations matrix is A^TWA , where

$$A_{ii} = \partial M_i / \partial x_i, \tag{8.3.1.4}$$

and W is a weight matrix. A constrained model, $M_i(\mathbf{z})$, maybe constructed using relations of the form

$$x_i = g_i(z_1, z_2, \dots, z_a).$$
 (8.3.1.5)

Applying the chain rule for differentiation, the normal-equations matrix for the constrained model is B^TWB , where

$$B_{ik} = \partial M_i(\mathbf{x})/\partial z_k = \sum_{j=1}^p \left[\partial M_i(\mathbf{x})/\partial x_j\right](\partial x_j/\partial z_k). \tag{8.3.1.6}$$

This may be written in matrix form $\mathbf{B} = \mathbf{AC}$, where $C_{jk} = \partial x_j/\partial z_k$ defines a $p \times q$ constraint matrix. The application of constraints involves (a) determination of the model to be used, (b) calculation of the elements of \mathbf{C} , and (c) computation of the modified normal-equations matrix.

The construction of matrix C by a procedure known as the variable reduction method may be presented formally as follows: Designate by Z the matrix whose elements are

$$Z_{jk} = \partial g_j(\mathbf{x})/\partial x_k, \qquad (8.3.1.7)$$

and partition Z in the form Z = (U, V), where V is composed of (p-q) columns of Z chosen to be linearly independent, so that V is nonsingular. [V is shown as the last (p-q) columns only for convenience. Any linearly independent set may be chosen.] The rows of Z form a basis for a (p-q)-dimensional subspace of the p-dimensional parameter space, and we wish to construct a basis for z, a q-dimensional subspace that is orthogonal to it, so that all shifts within that subspace starting at a point where the constraints are satisfied, a feasible point, leave the values of the constraint relations unchanged. This basis is used for the columns of C, which is given by

$$C = \begin{pmatrix} I_q \\ -V^{-1}U \end{pmatrix}. \tag{8.3.1.8}$$

In this formulation, the columns of V correspond to dependent parameters that are functions of the independent parameters corresponding to the columns of U.

Most existing programs provide for the calculation of the structure factor, F, and its partial derivatives with respect to a conventional set of parameters, including occupancy, position, isotropic or anisotropic atomic displacement factors, and possibly higher cumulants of an atomic density function (Prince, 1994). The constrained calculation is usually performed by evaluating selected elements, $\partial x_i/\partial z_k$. Because the constraint matrix is often extremely sparse, calculation of a limited sum involving only the nonzero elements is usually computationally superior to a full matrix multiplication. After adjustment of the z's, equations (8.3.1.5) are used to update the parameters. Using this procedure, it is not necessary to express the structure factor, or its derivatives, in terms of the refined parameters. This is particularly important when the constrained model involves arbitrary molecular shapes or rigid-body thermal motions.

The need for constraints arises most frequently when the crystal structure contains atoms in special positions. Here, certain parameters will be constant or linearly related to others. If a parameter is constrained to be a constant, the corresponding row of C will contain zeros, and that column will be ignored. When parameters are linearly dependent on others, which may occur in trigonal, hexagonal, tetragonal and cubic space groups, the modification indicated in (8.3.1.6) cannot be avoided. The constraint relationships among position parameters are trivial. Levy (1956) described an algorithm for determining the constraints that pertain to second and higher cumulants in the structure-factor formula. Table 8.3.1.1 is a summary of relations that are found for anisotropic atomic displacement factors, with a listing of the space groups in which they occur. Johnson (1970) provides a table listing the number of unique coefficients for each possible site symmetry for tensors of various ranks, which is useful information for verification of constraint relationships.

Another important use of constraints applies to the occupancies of certain sites in the crystal where, for example, a molecule is disordered in two or more possible orientations or (very common in minerals) several elements are distributed among several sites. In both cases, refinement of all of the fractional occupancies tends to be extremely ill conditioned, because of

$$\sum_{i=1}^{n} a_{ij} = 1. {(8.3.1.10)}$$

If necessary, vacancies may be included as one of the n species present. In theory, (8.3.1.9) and (8.3.1.10) could be solved for $(n-1)\times(m-1)$ unknown parameters, a_{ij} , with m+n-1 constraint relations, but, in practice, at most one occupancy factor per site can be refined. When constraints are applied, the correlations between occupancies and displacement factors are greatly reduced.

In the analysis of a crystal structure, it may be desirable to test various constraints on the shape or symmetry of a molecule. For example, the molecule of a particular compound may have orthorhombic symmetry in the liquid or vapour phase, but crystallize with a monoclinic or triclinic space group. Without constraints, it is impossible to determine whether the crystallization has caused changes in the molecular conformation. Residual errors in the observations will invariably lead to deviations from the original molecular geometry, but these may or may not be meaningful.

With molecular-shape constraints, it is possible to constrain the geometry to any desired conformation. The first step is to describe the molecule in a special, orthonormal coordinate system that has a well defined relationship between the coordinate axes and the symmetry elements. If this system is properly chosen, the description of the molecule is easy. The next step is to describe the transformation between this orthonormal system and the crystallographic axes. A standard, orthonormal coordinate system (Prince, 1994) can be constructed with its x axis parallel to a and its z axis parallel to \mathbf{c}^* . If the special system is translated with respect to the standard system so that they share a common origin, Eulerian angles, ω , χ , and φ , may be used to define a matrix that rotates the special coordinates into the standard system. Angle ω is defined as the clockwise rotation through which the special system must be rotated about the z axis of the standard system to bring the z axis of the special system into the x, z plane of the standard system. Similarly, angle χ is the clockwise angle through which the resulting, special system must be rotated about the y axis of the standard system to bring the z axes into coincidence, and, finally, angle φ is the clockwise angle through which the special system must be rotated about the common z axes to bring the other axes into coincidence. The overall transformation is given by

$$\mathbf{R} = \begin{pmatrix} \cos\varphi\cos\chi\cos\omega - \sin\varphi\sin\omega & \cos\varphi\cos\chi\sin\omega + \sin\varphi\cos\omega & -\cos\varphi\sin\chi \\ -\sin\varphi\cos\chi\cos\omega - \cos\varphi\sin\omega & -\sin\varphi\cos\chi\sin\omega + \cos\varphi\cos\omega & \sin\varphi\sin\chi \\ \sin\chi\cos\omega & \sin\chi\sin\omega & \cos\chi \end{pmatrix}. \tag{8.3.1.11}$$

high correlations between occupancies and atomic displacement parameters. The overall chemistry, however, may be known from electron microprobe (Finger, 1969) or other analytic techniques to much better precision than it is possible to determine it using diffraction data alone. The constraining equations for the occupancies of n species in m sites have the form

$$\sum_{i=1}^{m} b_i a_{ij} = p_j, \tag{8.3.1.9}$$

where b_i is the multiplicity of the *i*th site, a_{ij} is the fractional occupancy of the *j*th species in the *i*th site, and p is the total number of atoms of species j per unit cell. For a given crystal structure and composition, the bs and ps are known, and, furthermore, it is possible to write an additional constraint for the total occupancy of each site,

The overall transformation of a vector, \mathbf{x}' , from the special coordinate system to the crystallographic system is given by

$$\mathbf{x} = \mathbf{D}^{-1} \mathbf{R} \mathbf{x}' + \mathbf{t},$$
 (8.3.1.12)

where \mathbf{t} is the origin offset between the two systems and \mathbf{D} is the upper triangular Cholesky factor (Subsection 8.1.1.1) of the metric tensor, \mathbf{G} , which is defined by

$$\mathbf{G} = \begin{pmatrix} \mathbf{a} \cdot \mathbf{a} & \mathbf{a} \cdot \mathbf{b} & \mathbf{a} \cdot \mathbf{c} \\ \mathbf{a} \cdot \mathbf{b} & \mathbf{b} \cdot \mathbf{b} & \mathbf{b} \cdot \mathbf{c} \\ \mathbf{a} \cdot \mathbf{c} & \mathbf{b} \cdot \mathbf{c} & \mathbf{c} \cdot \mathbf{c} \end{pmatrix}. \tag{8.3.1.13}$$

Equations (8.3.1.12) are the constraint relationships, and the refinable parameters include the adjustable parameters in the special system, the origin offset, and the three rotation angles. This set of parameters, although it is written in a very different manner, is a linear transformation of a subset of the conventional

8.3. CONSTRAINTS AND RESTRAINTS IN REFINEMENT

Table 8.3.1.1. Symmetry conditions for second-cumulant tensors

If more than one condition is applicable for a space group, the site is identified by its Wyckoff notation following the space-group symbol. The stated conditions are valid only for the first equipoint listed for the position. For space groups with alternative choices of origin, the option with a centre of symmetry has been selected.

(A) Monoclinic

- (1) Site symmetry m, 2, 2/m four independent elements
 - (a) $\beta_{12} = \beta_{23} = 0$; one principal axis parallel to [010] All groups with unique axis b
 - (b) $\beta_{13} = \beta_{23} = 0$; one principal axis parallel to [001] All groups with unique axis c

(B) Orthorhombic

- (1) Site symmetry m, 2, 2/m four independent elements
 - (a) $\beta_{12} = \beta_{13} = 0$; one principal axis parallel to [100] P222(i,j,k,l), $P222_1(a,b)$, $C222_1(a)$, C222(e,f), F222(e,j), I222(e,f), $I2_12_12_1(a)$, Pmm2(g,h), $Pmc2_1$, Pma2(c), $Pmn2_1$, Cmm2(e), $Cmc2_1$, Amm2(d,e), Ama2(b), Fmm2(c), Imm2(d), Ima2(b), Pmmm(u,v), Pnnn(g,h), Pccm(i,j), Pban(g,h), Pmma(k), Pnna(d), Pmna(a,b,c,d,e,f,h), Pbcm(c), Pmmn(e), Cmcm(a,b,e,f), Cmca(a,b,d,f), Cmmm(n), Cccm(g), Cmma(c,d,h,i,m), Ccca(e), Fmmm(c,l,m), Fddd(e), Immm(l), Ibam(f), Ibca(c), Imma(a,b,f,h)
 - (b) $\beta_{12} = \beta_{23} = 0$; one principal axis parallel to [010] $P222(m,n,o,p), P222_1(c,d), C222_1(b), C222(g,h), F222(f,i), I222(g,h), I2_12_12_1(b), Pmm2(e,f), Cmm2(d), Amm2(c), Abm2(c), Fmm2(d), Imm2(c), Pmmm(w,x), Pnnn(i,j), Pccm(k,l), Pban(i,j), Pmma(a,b,c,d,g,h,i,j), Pmma(g), Pcca(c), Pmmm(f), Pbcn, Pnma, Cmca(e), Cmmm(o), Cccm(h), Cmma(e,f,j,k,n), Ccca(f), Fmmm(d,k,n), Fddd(f), Immm(m), Ibam(g), Ibca(d), Imma(c,d,g,i)$
 - (c) $\beta_{13} = \beta_{23} = 0$; one principal axis parallel to [001] $P222(q, r, s, t), P2_12_12, C222(i, j, k), F222(g, h), I222(i, j), I2_12_12_1(c), Pcc2, Pma2(a, b), Pnc2, Pba2, Pnn2, Cmm2(c), Ccc2, Abm2(a, b), Ama2(a), Aba2, Fmm2(b), Fdd2, Iba2, Ima2(a), Pmmm(y, z), Pnnn(k, l), Pccm(a, b, c, d, m, n, o, p, q), Pban(k, l), Pnna(c), Pcca(d, e), Pbam, Pccn, Pbcm(d), Pnnm, Cmcm(g), Cmmm(e, f, m, p, q), Cccm(c, d, e, f, i, j, k, l), Cmma(l), Ccca(g, h), Fmmm(e, j, o), Fddd(g), Immm(n), Ibam(c, d, h, i, j), Ibca(e)$
- (2) Site symmetry mm2, 222, mmm three independent elements
 - (a) $\beta_{12} = \beta_{13} = \beta_{23} = 0$ principal axes parallel to crystal axes All space groups

(C) Tetragonal

- (1) Site symmetry m, 2, 2/m four independent elements
 - (a) $\beta_{12} = \beta_{13} = 0$; one principal axis parallel to [100] $P422(l, m, n, o), P4_222(j, k, l, m), I422(h, i), I4_122(f), I4_1md, P\overline{4}2m(i, j, k, l), P\overline{4}2c(g, i), I\overline{4}2m(f, g), I\overline{4}2d(d), P4/mcc(k, l), P4/nbm(k, l), P4/nnc(i, j), P4/nmm(i), P4_2/mcm(l, m), P4_2/nbc(h, i), P4_2/nnm(i, j), P4_2/nmc(g), I4/mmm(n), I4/mcm(j), I4_1/amd(c, d, f, h), I4_1/acd(e)$
 - (b) $\beta_{12} = \beta_{23} = 0$; one principal axis parallel to [010] $P4_122(a,b), P4_322(a,b), P4mm(e,f), P4_2mc, I4mm(d), P42c(h,j), P4m2(j,k), I4m2(i), P4/mmm(s,t)$
 - (c) $\beta_{13} = \beta_{23} = 0$; one principal axis parallel to [001] P4, $P4_2$, P4, P4,
 - (d) $\beta_{11} = \beta_{22}$, $\beta_{13} = -\beta_{23}$ one principal axis parallel to [110] P422(j,k), $P42_12(e,f)$, $P4_122(c)$, $P4_12_12$, $P4_222(n,o)$, $P4_22_12(e,f)$, $P4_322(c)$, $P4_32_12$, I422(g,j), $I4_122(d)$, $P\overline{4}m2(h,i)$, $P\overline{4}c2(e,f)$, $P\overline{4}b2(g,h)$, $P\overline{4}n2(g)$, $I\overline{4}m2(g,h)$, $I\overline{4}c2(e,h)$, P4/mcc(j), P4/mbm(e,f,i,j,m), P4/mnc(h), P4/mnc(g), P4/mmc(h), P4/mnc(h), P4/mnc(h),
 - (e) $\beta_{11} = \beta_{22}$, $\beta_{13} = \beta_{23}$; one principal axis parallel to [1 $\overline{10}$] $I4_122(e)$, P4mm(d), P4bm, $P4_2cm(d)$, $P4_2nm(c)$, I4mm(c), I4cm, $P\overline{4}2m(n)$, $P\overline{4}2_1m(e)$, $P\overline{4}n2(f)$, $I\overline{4}2m(i)$, P4/mmm(r), P4/mbm(k), P4/nmm(d, e, g, h, j), P4/ncc(f), $P4_2/mcm(o)$, $P4_2/mnm(j)$, $P4_2/ncm(c)$, $P4_2/ncm(c, d, g, h, i)$, I4/mmm(f, m), I4/mcm(l)
- (2) Site symmetry mm2, 222, mmm three independent elements
 - (a) $\beta_{12} = \beta_{13} = \beta_{23} = 0$; principal axes parallel to crystal axes $P422, P4_222(a, b, c, d), I422(c), P4mm, P4_2mc, I4mm, I4_1md, P42m(e, f), P42c, P4m2, I4m2, I42m(c), P4/mmm(e, f, i, l, m, n, o), P4/mcc, P4/nnc, P4/nmm, P4_2/mmc, P4_2/mcm(e), P4_2/nbc(a, b), P4_2/nnm(c), P4_2/nmc, I4/mmm(c, g, i, j), I4_1/amd$

8. REFINEMENT OF STRUCTURAL PARAMETERS

Table 8.3.1.1. Symmetry conditions for second-cumulant tensors (cont.)

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(C) Tetragonal (cont.)
                   (b) \beta_{11} = \beta_{22}, \beta_{13} = \beta_{23} = 0; principal axes parallel to [110], [1\overline{10}] and [001]
                                      P42,2, P4,22(e,f), P4,2,2, I422(d), I4,22, P4bm, P4,cm, P4,cm, I4cm, P42m(g,h), P42,m, P4c2, P4b2, P4b2, P4n2, I4c2, I42m(e),
                                    P4/mmm(j,k), P4/nbm, P4/mbm, P4/mnc, P4/ncc, P4_2/mcm(a,c,g,h,i,j), P4_2/nbc(c), P4_2/nnm(d,g), P4_2/mbc, P4_2/mnm,
                                    P4_2/ncm, I4/mmm(h), I4/mcm, I4_1/acd
(3) Site symmetry 4, \overline{4}, 4/m, 4mm, \overline{4}2m, 422, 4/mmm – two independent elements
                   (a) \beta_{11} = \beta_{22}, \beta_{12} = \beta_{13} = \beta_{23} = 0; uniaxial with unique axis parallel to [001]
                                     All space groups
(D) Trigonal (hexagonal axes) and hexagonal
(1) Site symmetry m, 2, 2/m – four independent elements
                   (a) \beta_{13} = \beta_{23} = 0; one principal axis parallel to [001]
                                     P6, P6, P6, P6, P6/m, P6/m, P6/m, P622(i), P6/22(e, f), P6/22(e, f), P6cc, P6/m2(l, m), P6/c2(k), P6/m2(l, k), P6/m2(l, 
                                    P6/mmm(p,q), P6/mcc(g,i,l), P6_3/mcm(j), P6_3/mmc(j)
                  (b) \beta_{11}=\beta_{22},\ \beta_{13}=-\beta_{23} one principal axis parallel to [110]
                                    P3m1, R3m, P\overline{3}m1(i), R\overline{3}m(h), P6mm(e), P6_3mc, P\overline{6}m2(n)
                  (c) \beta_{11} = \beta_{22}, \beta_{13} = \beta_{23}; one principal axis parallel to [2\overline{10}]
                                    P312, P3_112, P3_212, P\overline{3}1m(i, j), P\overline{3}1c, P622(l, m), P\overline{6}c2(j)
                   (d) \beta_{22} = 2\beta_{12}, 2\beta_{13} = \beta_{23}; one principal axis parallel to [100]
                                     P321, P3_121, P3_221, R32, P\overline{3}m1(e, f, g, h), P\overline{3}c1, R\overline{3}m(d, e, f, g), R\overline{3}c, P622(j, k), P6_122(a), P6_522(a), P6_222(g, h), P6_422(g, h), P6_422(g, h), P6_522(g, h), P6_522(
                                    P6_322(g), P\overline{6}2c(g), P6/mmm(o), P6/mcc(j), P6_3/mmc(g, i, k)
                   (e) \beta_{22} = 2\beta_{12}, \beta_{23} = 0; one principal axis parallel to [210]
                                     P31m, P\overline{3}1m(f,g,k), P6_122(b), P6_522(b), P6_522(i,j), P6_422(i,j), P6_322(h), P6mm(d), P6_3cm, P\overline{6}2m(i), P6/mmm(n),
                                    P6/mcc(k), P6_3/mcm(f, i, k)
(2) Site symmetry mm2, 222, mmm - three independent elements
                   (a) \beta_{22} = 2\beta_{12}, \beta_{13} = \beta_{23} = 0; principal axes parallel to [100] and [001]
                                    P622, P6<sub>2</sub>22, P6<sub>4</sub>22, P6mm, P<del>6</del>02m, P6/mmm, P6/mcc, P6<sub>3</sub>/mcm, P6<sub>3</sub>/mmc
                   (b) \beta_{11} = \beta_{22}, \beta_{13} = \beta_{23} = 0; principal axes parallel to [110], [\overline{210}] and [001]
                                    P\overline{6}m2
(3) Site symmetry 3, \overline{3}, 3m, 32, \overline{3}m, \overline{6}, 6, 6/m, \overline{6}m2, 6mm, 622, 6/mmm – two independent elements
                   (a) \beta_{11} = \beta_{22} = 2\beta_{12}, \beta_{13} = \beta_{23} = 0; unique axis parallel to c
                                    All space groups
(E) Cubic
(1) Site symmetry m, 2, 2/m – four independent elements
                   (a) \beta_{12} = \beta_{13} = 0; one principal axis parallel to [100]
                                      P23, F23, I23, I2_13, Pm\overline{3}, Pm\overline{3}, Fm\overline{3}, Fm\overline{3}, Fd\overline{3}, Im\overline{3}, Ia\overline{3}, P432(h), P4_232(h, i, j), F432(i), F4_132(f), I432(g), I4_132(f), P\overline{4}3m(h), P4_232(h, i, j), P4_332(h, i, j), P
                                    I\overline{4}3m(f), P\overline{4}3n, F\overline{4}3c, I\overline{4}3d, Pm\overline{3}m(k, l), Pn\overline{3}n(g), Pm\overline{3}n(k), Pn\overline{3}m(h), Fm\overline{3}m(j), Fm\overline{3}c(i), Fd\overline{3}c(f), Im\overline{3}m(j), Ia\overline{3}d(f)
                   (b) \beta_{11} = \beta_{22}, \beta_{13} = \beta_{23}; one principal axis parallel to [1\overline{10}]
                                    P\overline{4}3m(i), F\overline{4}3m, I\overline{4}3m(g), Pm\overline{3}m(m), Pn\overline{3}m(k), Fm\overline{3}m(k), Fd\overline{3}m(g), Im\overline{3}m(k)
                   (c) \beta_{22} = \beta_{33}, \beta_{12} = -\beta_{13}; one principal axis parallel to [011]
                                    P432(i,j), P4_232(l), F432(g,h), I432(h), P4_132, I4_132(g), Pn\overline{3}n(h), Pm\overline{3}n(j), Pn\overline{3}m(j), Fm\overline{3}c(h)
                  (d) \beta_{22} = \beta_{33}, \beta_{12} = \beta_{13}; one principal axis parallel to [01\overline{1}]
                                    P4_232(k), F4_132(g), I432(i), P4_332, I4_132(h), Pn\overline{3}m(i), Fd\overline{3}m(h,i), Fd\overline{3}c(g), Im\overline{3}m(i), Ia\overline{3}d(g)
(2) Site symmetry mm2, 222, mmm - three independent elements
                  (a) \beta_{12} = \beta_{13} = \beta_{23} = 0; principal axes parallel to crystal axes
                                    P23, I23, Pm\overline{3}, Pn\overline{3}, Fm\overline{3}, Im\overline{3}, P4_232(d), P\overline{4}3n, Pm\overline{3}m(h), Pm\overline{3}n, Fm\overline{3}c, Im\overline{3}m(g)
                   (b) \beta_{22} = \beta_{33}, \beta_{12} = \beta_{13} = 0; principal axes parallel to [011], [01\overline{1}] and [100]
                                    P4_{2}32(e,f), F432, I432, I4_{1}32, P\overline{4}3m, F\overline{4}3m, I\overline{4}3m, Pm\overline{3}m(i,j), Pn\overline{3}m, Fm\overline{3}m, Fd\overline{3}m, Im\overline{3}m(h), Ia\overline{3}d
(3) Site symmetry 3, \overline{3}, 3m, 32, \overline{3}m, \overline{6}, 6, 6/m, \overline{6}m2, 6mm, 622, 6/mmm – two independent elements
                   (a) \beta_{11} = \beta_{22} = \beta_{33}, \beta_{12} = \beta_{13} = \beta_{23}; unique axis parallel to [111]
                                    All space groups
(4) Site symmetry 4, \overline{4}, 4/m, 4mm, \overline{4}2m, 422, 4/mmm – two independent elements
                  (a) \beta_{22} = \beta_{33}, \beta_{12} = \beta_{13} = \beta_{23} = 0; uniaxial with unique axis parallel to [100]
                                    All space groups
(5) Site symmetry 23, m3, \overline{4}3m, 432, m3m – one independent element
                   (a) \beta_{11} = \beta_{22} = \beta_{33}, \beta_{12} = \beta_{13} = \beta_{23} = 0; isotropic
                                    All space groups
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crystallographic parameters, so that statistical tests based on the F ratio or Hamilton's R ratio (Section 8.4.2; Hamilton, 1964) may be used to assess significance. Shape constraints differ from those owing to space group or chemical conditions in that the constraint equations (8.3.1.12) are not linear functions of the independent parameters. Thus, the elements of C are not constants and must therefore be evaluated in each iteration of the refinement algorithm.

Another area in which application of constraints is important arises whenever some portion of the structure undergoes thermal motion as a rigid entity. One means of determining rigid-motion parameters is to refine the conventional, anisotropic atomic displacement factors of all atoms individually and to fit a librational model to the resulting thermal factors (Schomaker & Trueblood, 1968). A problem arises with this approach because the presence of libration implies curvilinear motion in the crystallographic system, and thus the probability density function for an atom that does not lie on the axis of libration cannot be described by a Gaussian function in a rectilinear coordinate system. For neutron diffraction, where H atoms have major scattering power, the effect may be large enough to affect convergence (Prince, Dickens & Rush, 1974). Anharmonic (third-cumulant) terms could be used, but the number of parameters increases rapidly, because there are as many as ten, independent, third cumulant tensor elements per

Thermal motions of rigid bodies are represented by a symmetric, translation tensor, **T**, a symmetric, libration tensor, **L**, and a nonsymmetric, screw correlation tensor, **S** (Cruickshank, 1961; Schomaker & Trueblood, 1968). Any sequence of rotations of a rigid body about a fixed point is equivalent to a single, finite rotation about some axis passing through the fixed point. This rotation can be represented (Prince, 1994) by an axial vector, λ , where $|\lambda|$ is the magnitude of the rotation, and the direction cosines of the axis with respect to some system of orthogonal axes are given by $\alpha_i = \lambda_i/|\lambda| = \lambda_i/(\lambda_1^2 + \lambda_2^2 + \lambda_3^2)^{1/2}$. An exact expression for the displacement, **u**, of a point in the rigid body, located by a vector **r** from the centre of mass, owing to a rotation λ about an axis passing through the centre of mass is

$$\mathbf{u} = (\sin|\lambda|/|\lambda|)(\lambda \times \mathbf{r}) + [(1 - \cos|\lambda|)/|\lambda|^2][\lambda \times (\lambda \times \mathbf{r})].$$
(8.3.1.14)

For small rotations, the trigonometric functions can be replaced by power-series expansions, and, because of the extremely rapid convergence of these series, (8.3.1.14) is approximated extremely well, even for values of $|\lambda|$ as large as 0.5 rad, by

$$\mathbf{u} = (1 - |\lambda|^2 / 6)(\lambda \times \mathbf{r}) + [(1/2) - |\lambda|^2 / 24][\lambda \times (\lambda \times \mathbf{r})].$$
(8.3.1.15)

By expansion of the vector products, this can be written

$$u_{i} = \sum_{j=1}^{3} \left(A(\mathbf{r})_{ij} \lambda_{j} + \sum_{k=1}^{3} \left\{ B(\mathbf{r})_{ijk} \lambda_{j} \lambda_{k} + \sum_{l=1}^{3} \left[C(\mathbf{r})_{ijkl} \lambda_{j} \lambda_{k} \lambda_{l} + \sum_{m=1}^{3} D(\mathbf{r})_{ijklm} \lambda_{j} \lambda_{k} \lambda_{l} \lambda_{m} \right] \right\} \right),$$

$$(8.3.1.16)$$

where the coefficients, $A(\mathbf{r})_{ij}$, $B(\mathbf{r})_{ijk}$, $C(\mathbf{r})_{ijkl}$, and $D(\mathbf{r})_{ijklm}$ are multiples of components of \mathbf{r} . For example, $[\lambda \times \mathbf{r}]_1 = \lambda_2 r_3 - \lambda_3 r_2$, so that $A(\mathbf{r})_{11} = 0$, $A(\mathbf{r})_{12} = r_3$, and $A(\mathbf{r})_{13} = -r_2$. These coefficients have been tabulated by Sygusch (1976), and expressed in Fortran source code by Prince (1994).

If the centre of mass of the rigid body also moves, the total displacement of the point at \mathbf{r} is $\mathbf{v} = \mathbf{u} + \mathbf{t}$, where \mathbf{t} is the displacement of the centre of mass from its equilibrium

position. A discussion of the effects of rigid-body motion on diffraction intensities involves quantities like $\langle v_i \rangle$, $\langle v_i v_j \rangle$, and so forth, the ensemble averages of these quantities over many unit cells, which may be assumed to be equal to the time averages for one unit cell over a long time. The rigid-body-motion tensors are defined by $T_{ij} = \langle t_i t_j \rangle$, $L_{ij} = \langle \lambda_i \lambda_j \rangle$, and $S_{ij} = \langle \lambda_i t_j \rangle$. The distributions of t_i and λ_i can usually be assumed to be approximately Gaussian, so that fourth moments can be expressed in terms of second moments. Thus, $\langle \lambda_i \lambda_j \lambda_k \lambda_l \rangle = L_{ij} L_{kl} + L_{ik} L_{jl} + L_{il} L_{jk}$, $\langle \lambda_i \lambda_j t_k t_l \rangle = L_{ij} T_{kl} + S_{ik} S_{jl} + S_{il} S_{jk}$, and so forth. If the elements of t and t are measured with respect to their mean positions, $t_i = \langle \lambda_i \rangle = 0$. Third moments, quantities like $t_i = 0$ and not necessarily vanish, except when the rigid body is centrosymmetric, but their effects virtually always are small, and can be neglected.

A particle that is part of a librating, rigid body undergoes a curvilinear motion that results in its having a mean position that is displaced from its equilibrium position. This causes an apparent shortening of interatomic distances, which must be corrected for if accurate values of bond lengths are to be derived. The displacement, **d**, from the equilibrium position to the mean position is (Prince & Finger, 1973)

$$d_{i} = \left\langle v_{i} \right\rangle = \sum_{j=1}^{3} \sum_{k=1}^{3} \left[B(\mathbf{r})_{ijk} L_{jk} + \sum_{l=1}^{3} \sum_{m=1}^{3} D(\mathbf{r})_{ijklm} (L_{jk} L_{lm} + L_{jl} L_{km} + L_{jm} L_{kl}) \right].$$
(8.3.1.17)

Anisotropic atomic displacement factors, β_{ij} , B_{ij} , or U_{ij} , are related by simple, linear transformations that are functions of the unit-cell constants to the quantity $\kappa_{ij} = \langle v_i v_j \rangle - \langle v_i \rangle \langle v_j \rangle$. If the rigid body has a centre of symmetry, so that the elements of **S** vanish, this is given by

$$\kappa_{ij} = T_{ij} + \sum_{k=1}^{3} \sum_{l=1}^{3} \left(A(\mathbf{r})_{ik} A(\mathbf{r})_{jl} L_{kl} + \sum_{m=1}^{3} \sum_{n=1}^{3} \left\{ 3[A(\mathbf{r})_{ik} C(\mathbf{r})_{jlmn} + A(\mathbf{r})_{jk} C(\mathbf{r})_{ilmn}] + 2B(\mathbf{r})_{ikm} B(\mathbf{r})_{jln} \right\} L_{kl} L_{mn} \right).$$
(8.3.1.18)

Expressions including elements of **S** have been given by Sygusch (1976) and, in Fortran source code, by Prince (1994). Expressions for anisotropic atomic displacement factors in terms of **T**, **L**, and **S** that included only terms linear in the tensor elements were given by Schomaker & Trueblood (1968), who pointed out that the diagonal elements of **S** never appeared individually, but only as the differences of pairs, so that the expressions were invariant under the addition of a constant to all three elements. This 'trace of **S** singularity' was resolved by applying the additional constraint $S_{11} + S_{22} + S_{33} = 0$. As was pointed out by Sygusch (1976), the inclusion of terms that are quadratic in the tensor elements removes this indeterminacy, but the effects of the additional terms are so small that the problem remains extremely ill conditioned. In practice, therefore, these elements should still be treated as underdetermined.

Prince (1994) lists the symmetry restrictions for each type of tensor for various point groups. Although the description of thermal motion is essentially harmonic within the rigid-body system, the structure-factor formulation must include what appear to be anharmonic terms. Prince also presents computer routines that contain the relations between the elements of T, L, and S and the second- and third-cumulant tensor elements. As in

the case of shape constraints, the equations are nonlinear, and the elements of C must be re-evaluated in each iteration.

8.3.2. Stereochemically restrained least-squares refinement

The precision with which an approximately correct model can be refined to describe the atomic structure of a crystal depends on the ability of the model to represent the atomic distributions and on the quality of the observational data being fitted with the model. In addition, although the structure can in principle be determined by a well chosen data set only a little larger than the number of parameters to be determined (Section 8.4.4), in practice, with a nonlinear model as complex as that for a macromolecular crystal, it is necessary for the parameters defining the model to be very much overdetermined by the observations. For well ordered crystals of small- and intermediate-sized molecules, it is usually possible to measure a hundred or more independent Bragg reflections for each atom in the asymmetric unit. When the model contains three position parameters and six atomic displacement parameters for each atom, the over-determinacy ratio is still greater than ten to one. In such instances, each model parameter can usually be quite well determined, and will provide an accurate representation of the average structure in the crystal, except in regions where ellipsoids are not adequate descriptions of the atomic distributions. This contrasts sharply with studies of biological macromolecules, in which positional disorder and thermal motion in large regions, if not the entire molecule, often limit the number of independent reflections in the data set to fewer than the number of parameters necessary to define the distributions of individual atoms. This problem may be overcome either by reducing the number of parameters describing the model or by increasing the number of independent observations. Both approaches utilize knowledge of stereochemistry.

A great deal of geometrical information with which an accurate model must be consistent is available at the onset of a refinement. The connectivity of the atoms is generally known, either from the approximately correct Fourier maps of the electron density obtained from a trial structure determination or from sequencing studies of the molecules. Quite tight bounds are placed on local geometry by the accumulating body of information concerning bond lengths, bond angles, group planarity, and conformational preferences in torsion angles. Additional knowledge concerns van der Waals contact potential functions and hydrogen-bonding properties, and displacement factors must also be correlated in a manner consistent with the known geometry. In Section 8.3.1, we discuss the use of constraints to introduce this stereochemical knowledge. In this section, we discuss a technique that introduces the stereochemical conditions as additional observational equations (Waser, 1963). This method differs from the other in that information is introduced in the form of distributions about mean values rather than as rigidly fixed geometries. The parameters are restrained to fall within energetically permissible bounds.

8.3.2.1. Stereochemical constraints as observational equations

As described in Section 8.1.2, given a set of observations, y_i , that can be described by model functions, $M_i(\mathbf{x})$, where \mathbf{x} is the vector of model parameters, we seek to find \mathbf{x} for which the sum

$$S = \sum_{i=1}^{n} w_i [y_i - M_i(\mathbf{x})]^2$$
 (8.3.2.1)

is minimum. For restrained refinement, S is composed of several classes of observational equations, including, in addition to the ones for structure factors, equations for interatomic distances, planar groups and displacement factors.

Structure factors yield terms in the sum of the form

$$\Delta_{\rm SF} = \left[|F_{\rm obs}(\mathbf{h})| - |F_{\rm calc}(\mathbf{h})| \right]^2 / \sigma_{\mathbf{h}}^2. \tag{8.3.2.2}$$

The distances between bonded atoms and between next-nearest-neighbour atoms may be used to require bonded distances and angles to fall within acceptable ranges. This gives terms of the form

$$\Delta_d = (d_{\text{ideal}} - d_{\text{model}})^2 / \sigma_d^2, \tag{8.3.2.3}$$

where σ_d is the standard deviation of an empirically determined distribution of values for distances of that type. Groups of atoms may be restrained to be near a common plane by terms of the form (Schomaker, Waser, Marsh & Bergman, 1959)

$$\Delta_p = (\mathbf{m}_l \cdot \mathbf{r} - d_l)^2 / \sigma_p^2, \tag{8.3.2.4}$$

where \mathbf{m}_l and d_l are parameters of the plane, σ_p is again an empirically determined standard deviation, and \cdot indicates the scalar product.

If a molecule undergoes thermal oscillation, the displacement parameters of individual atoms that are stereochemically related must be correlated. These parameters may be required to be consistent with the known stereochemistry by assuming a model that gives a distribution function for the interatomic distances in terms of the individual atom parameters and then restraining the variance of that distribution function to a suitably small value. The variation with time of the distances between covalently bonded atoms can be no greater than a few hundredths of an ångström. Therefore, the thermal displacements of bonded atoms should be very similar along the bond direction, but they may be more dissimilar perpendicular to the bond. If we make the assumption that the atom with a broader distribution in a given direction is 'riding' on the atom with the narrower distribution, the variance of the interatomic distance parallel to a vector v making an angle $\theta(\mathbf{v}, i)$ with the direction of bond i is (Konnert & Hendrickson, 1980)

$$V_{\mathbf{v}} = \Delta_{\mathbf{v}}^{2} \cos^{2} \theta + (\Delta_{\mathbf{v}}^{4}/2d_{0}^{2})(\sin^{4} \theta - 6\sin^{2} \theta \cos^{2} \theta) + \dots,$$
(8.3.2.5)

where d_0 is the normal distance for that type of bond, $\Delta_{\bf v}^2=(\overline{u}_a^2-\overline{u}_b^2)$, and \overline{u}_a^2 and \overline{u}_b^2 are the mean square displacements parallel to ${\bf v}$ of atom a and atom b, respectively. The restraint terms then have the form $V_{\bf v}^2/\sigma_{\bf v}^2$. For isotropic displacement factors, these terms take the particularly simple form $(B_a-B_b)^2/\sigma_B^2$, but with the disadvantage that, when isotropic displacement parameters are used, the displacements cannot be suitably restrained along the bonds and perpendicular to the bonds simultaneously.

Several additional types of restraint term have proved useful in restraining the coordinates for the mean positions of atoms in macromolecules. Among these are terms representing non-bonded contacts, torsion angles, handedness around chiral centres, and noncrystallographic symmetry (Hendrickson & Konnert, 1980; Jack & Levitt, 1978; Hendrickson, 1985). Contacts between nonbonded atoms are important for determining the conformations of folded chain molecules. They may be described by a potential function that is strongly repulsive when the interatomic distance is less than some minimum value, but only weakly attractive, so that it can be neglected in practice, when the distance is greater than that value. This leads to terms of the form